

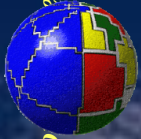
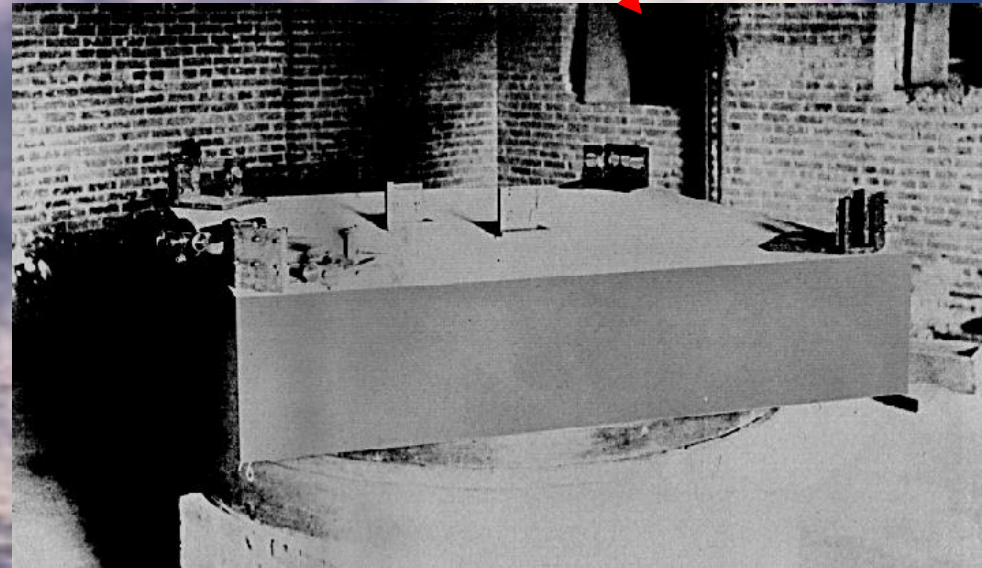
# Climate Research Directions

A dramatic sky with a bright sun breaking through a thick layer of clouds, creating a sunburst effect. The sun is positioned in the lower right quadrant, casting a strong light that illuminates the surrounding clouds and creates a lens flare. The clouds are dense and layered, with some appearing as soft, white wisps and others as darker, more textured masses. The overall color palette is dominated by deep blues and purples, with the bright yellow and white of the sun providing a stark contrast.

# A scientific consideration of climate (I)

Crucial experiments like the famous experiment of Michelson e Morley are not possible in climate science

How is it possible a scientific investigation of climate ?

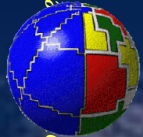


# A scientific consideration of climate (II)

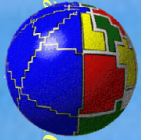
We can make experiments if we represent the climate system via a set of mathematical relations: the equation of climate.

The equations of climate are very difficult, but they can be solved by numerical methods.

We can then treat very complex mathematical equations, paying the price of an enormous number of elementary operations.



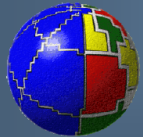
*The next generation of numerical models will be like new, more powerful, telescopes or particle accelerators and they will allow us to look further into the working of the Earth climate more accurately, extensively and reliably.*



*Euro Mediterranean*

*Center*

*for Climate Change*





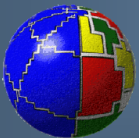
# The Mission

**Improve our understanding of the nature and mechanisms of climate variability, its causes and its impacts, with a special emphasis on the Mediterranean Area and its interactions with the global climate.** Major research themes will include tropical-extratropical teleconnections, decadal and interdecadal climate variability and the issues linked to the general circulation.

**Develop high quality products that will be made available to the scientific community, with an adequate user support, documentation and training.** Research will support the improvement of the CMCC products and guarantee a continuous high quality level.

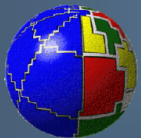
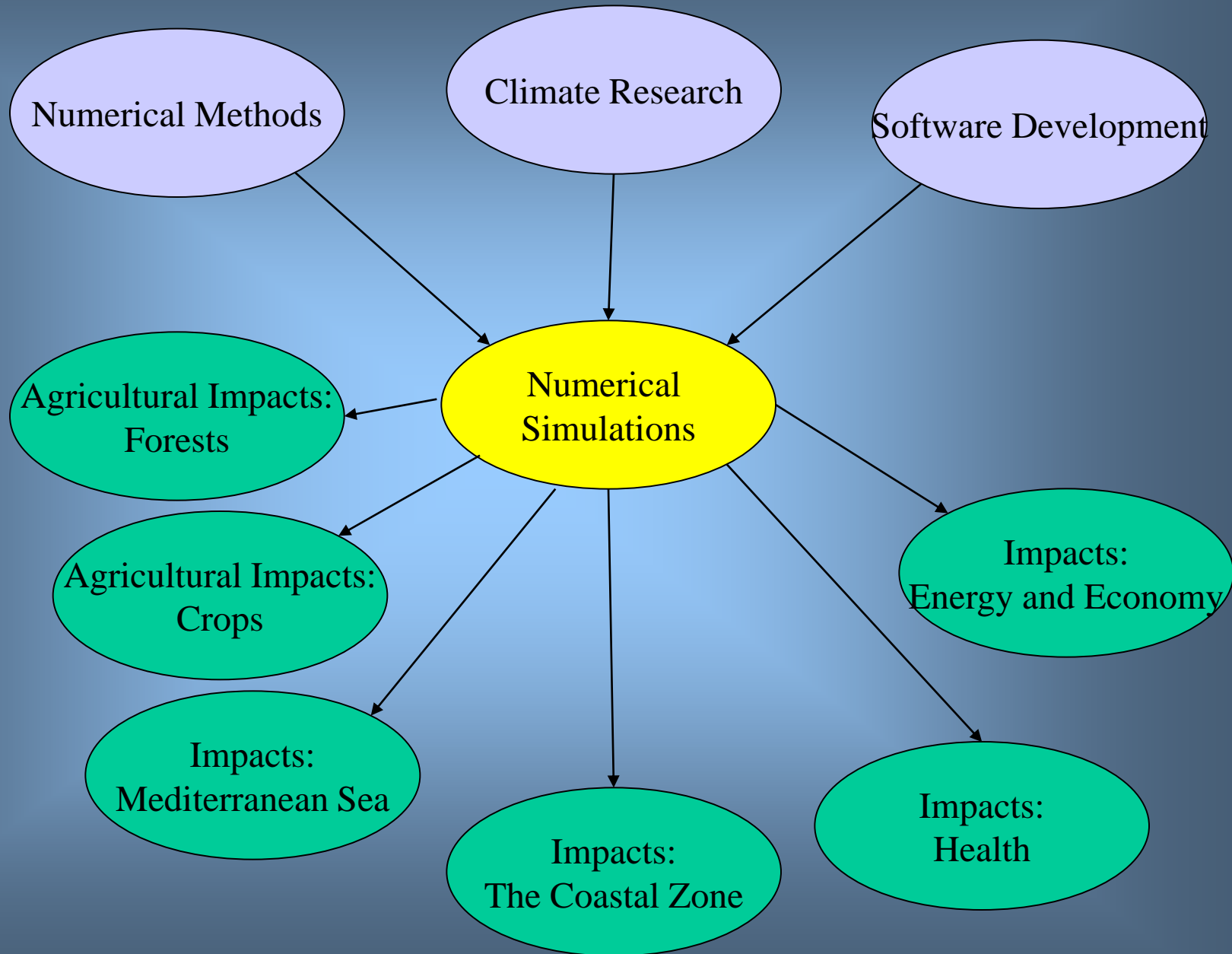
**Establish a significant computational facility** to support italian climate numerical simulation research and contribute to capacity building in the Mediterranean region

**Produce numerical models, simulations, applications and assessments.** CMCC will also perform high level training in the areas of climate dynamics and its impacts.





# The Structure of the CMCC



# CMCC-INGV planned scenario simulations:

- High-resolution, short-term (decadal) prediction experiments
- Long scenario simulations with the Carbon Cycle



## High-resolution, short-term (decadal) prediction experiments

- Ensemble of integrations of the period 1965-2035 with start dates every 5 years (1965, 1970, ..., 2005) and 3 member for each start date;
- Oceanic initial conditions: Ocean Analysis (CMCC-INGV) with observed anomalies on top of model climatology;
- Atmospheric ini. cond.: AMIP run;
- Sea-Ice ini. cond.: Ocean Analysis for the sea-ice cover distribution and model climatology for the sea-ice thickness;
- Prescribed GHGs and aerosols from observations for 1965-2005 and from scenarios (according to CMIP5) for 2005-2035;

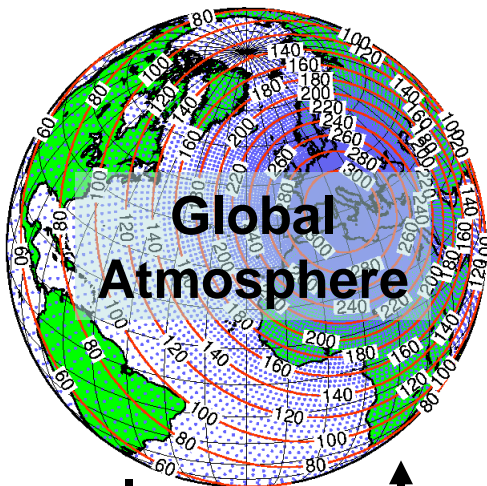
(Start by the end of 2009)

## Long-term (centennial) projection experiments with the Carbon Cycle Earth System Model

- Past Control Run and Historical (1850-2005) experiment
- Idealized 1% year experiment
- Prescribed GHGs and aerosols from observations for 1965-2005 and from scenarios (according to CMIP5, RCP4.5 and RCP8.5) for 2005-2100;.
- Hibbard et al (2007) design: Specified CO<sub>2</sub> concentration, save the land and ocean carbon fluxes to compute implied emission;.

# High-resolution, short-term (decadal) prediction experiments

## The high resolution CMCC-MODEL



**ATMOSPHERE** (dynamics, physics,  
prescribed gases and aerosols)

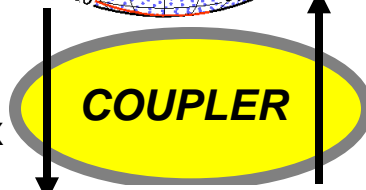
**ECHAM5 T159 - L31**

Roeckner et al. (2006)

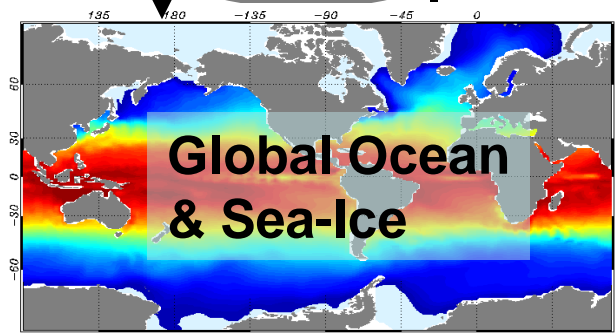
(T63-L95 stratosphere resolving)

(Manzini et al. 2006)

Heat Flux  
Water Flux  
Momentum Flux



SST  
Sea-ice



**OCEAN** (dynamics and physics)

**NEMO/ORCA2** (Barnier et al. 2006)

**SEA-ICE: LIM** (Timmermann et al. 2005)

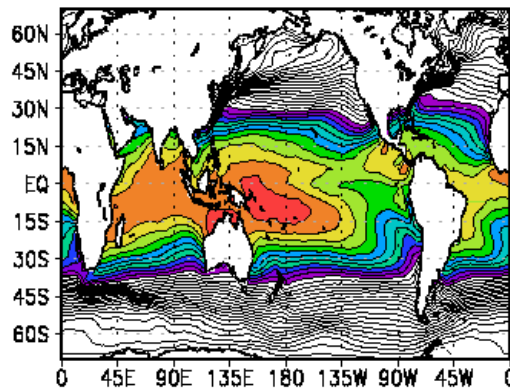
# High-resolution, short-term (decadal) prediction experiments

Preliminary results from a 20th Century simulation

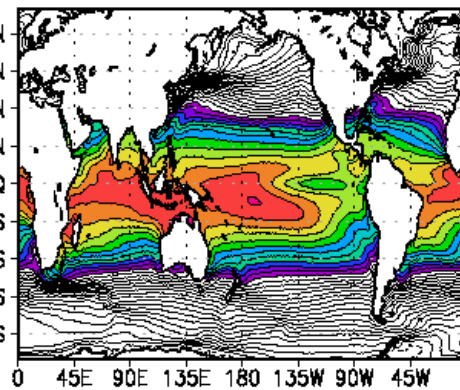
Mean SST 1951-2000

JFM

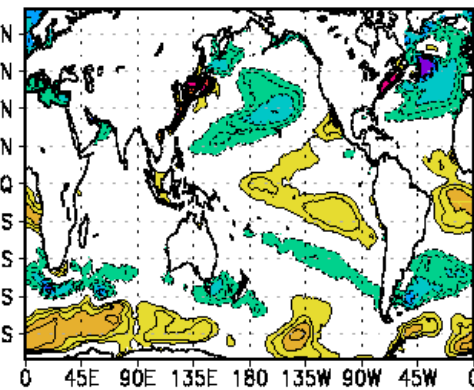
OBS (HadISST)



MODEL

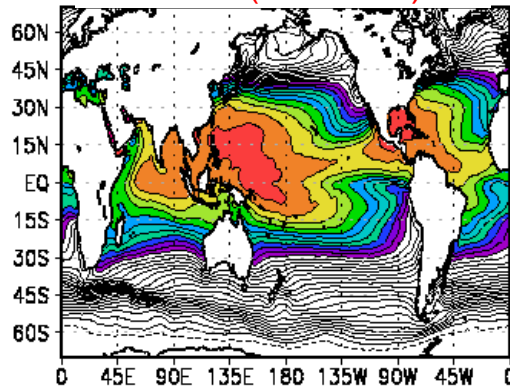


MODEL - OBS

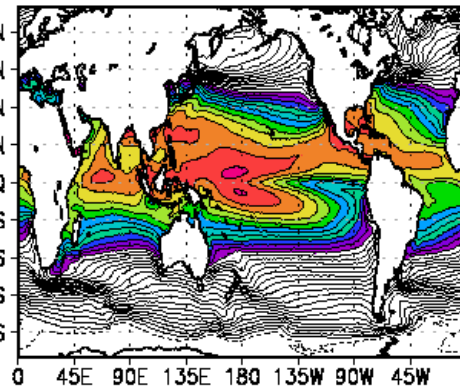


JAS

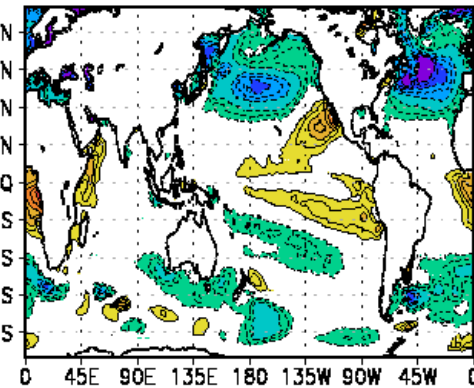
OBS (HadISST)



MODEL



MODEL - OBS



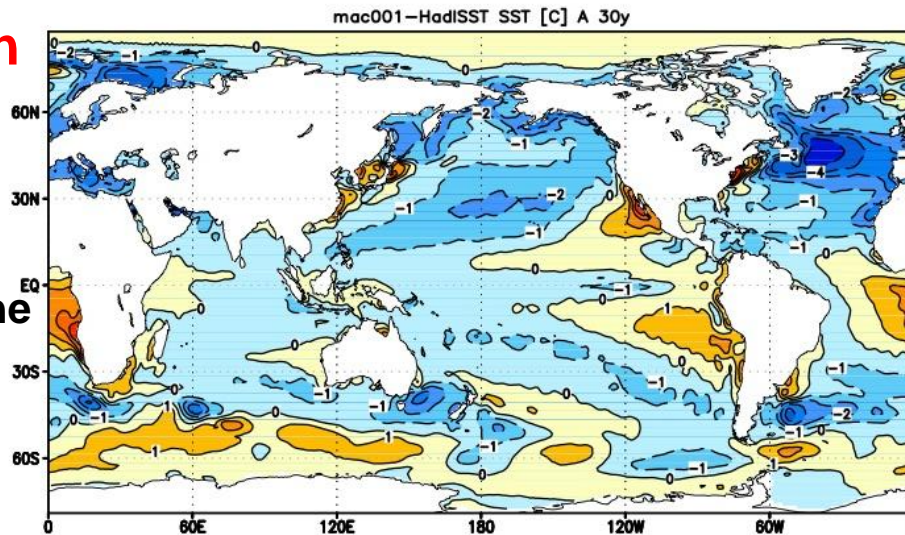
# CMCC Atmosphere Ocean Model + Stratosphere

**ECHAM5@T63L95, top at 80 km** (Manzini et al 2006, Giorgetta et 2006, Cagnazzo et al 2007)

## Present Control: 130-year Simulations

**Annual Mean  
SST [K]  
Model-OBS**

(Model: 30-yr  
average from the  
130 year run;  
OBS: 30-yr  
HadSST)



ATMOSPHERE  
ECHAM5



COUPLER  
OASIS



OCEAN/SEA ICE  
OPA8.2/LIM

*Planned (part of the COMBINE EC project):*

- *Past Control Run and 3 Ensembles of 10-year Hindcasts Runs*
- *Near-Term Potential Predictability Runs (3x10; RCP4.5)*

# *CMCC/INGV Carbon Earth System Model*

**ATMOSPHERE** (dynamics, physics,  
prescribed gases and aerosols)

**ECHAM4/5** (Roecker et al 1996, 2003)

**LAND, VEGETATION and  
TERRESTRIAL CARBON**

**SILVA** (Alessandri, 2006; Zeng et al 2004; Ducoudre et al 1993)

**Oasis 2/3 Coupler**  
(Valcke et al 2004)

**Marine Biogeochemistry  
and Ocean Carbon:**

**PELAGOS** (Vichi et al 2006a,b)

**Ocean** (dynamics and physics)

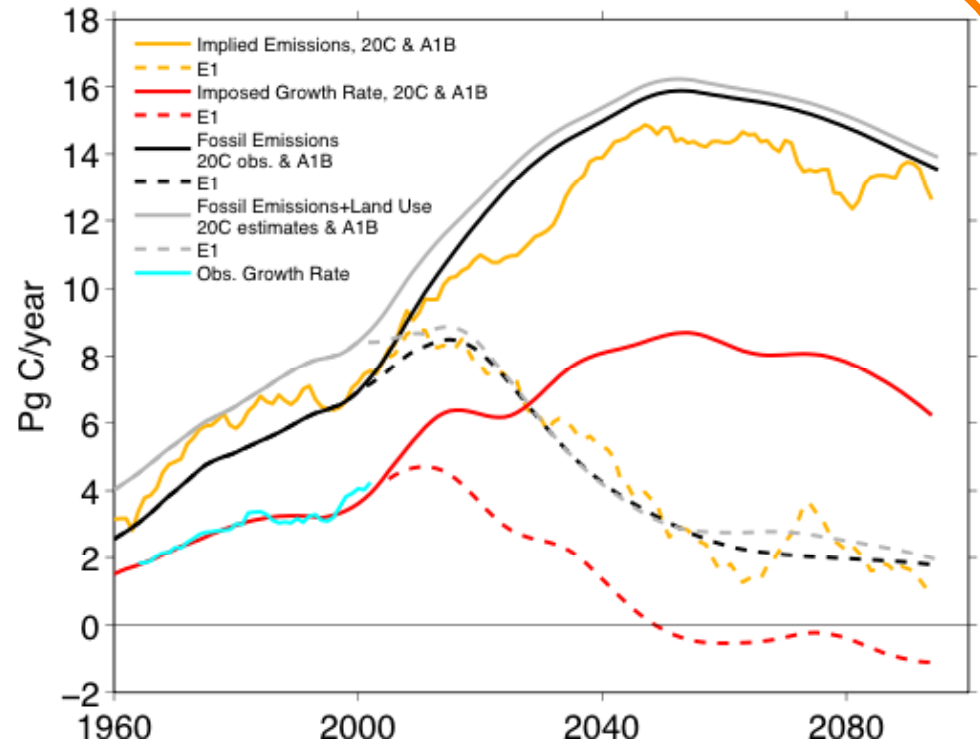
**OPA8.2/NEMO** (Madec et al 1998)

**SeaIce: LIM** (Timmermann et al 2005)



The CMCC/INGV Carbon ESM has been used in the ENSEMBLES exploratory runs (Johns et al, in preparation), with the Hibbard et al (2007) design applied to the A1B and E1 scenarios .

### Implied Emissions from the CMCC/INGV Carbon ESM



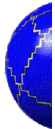
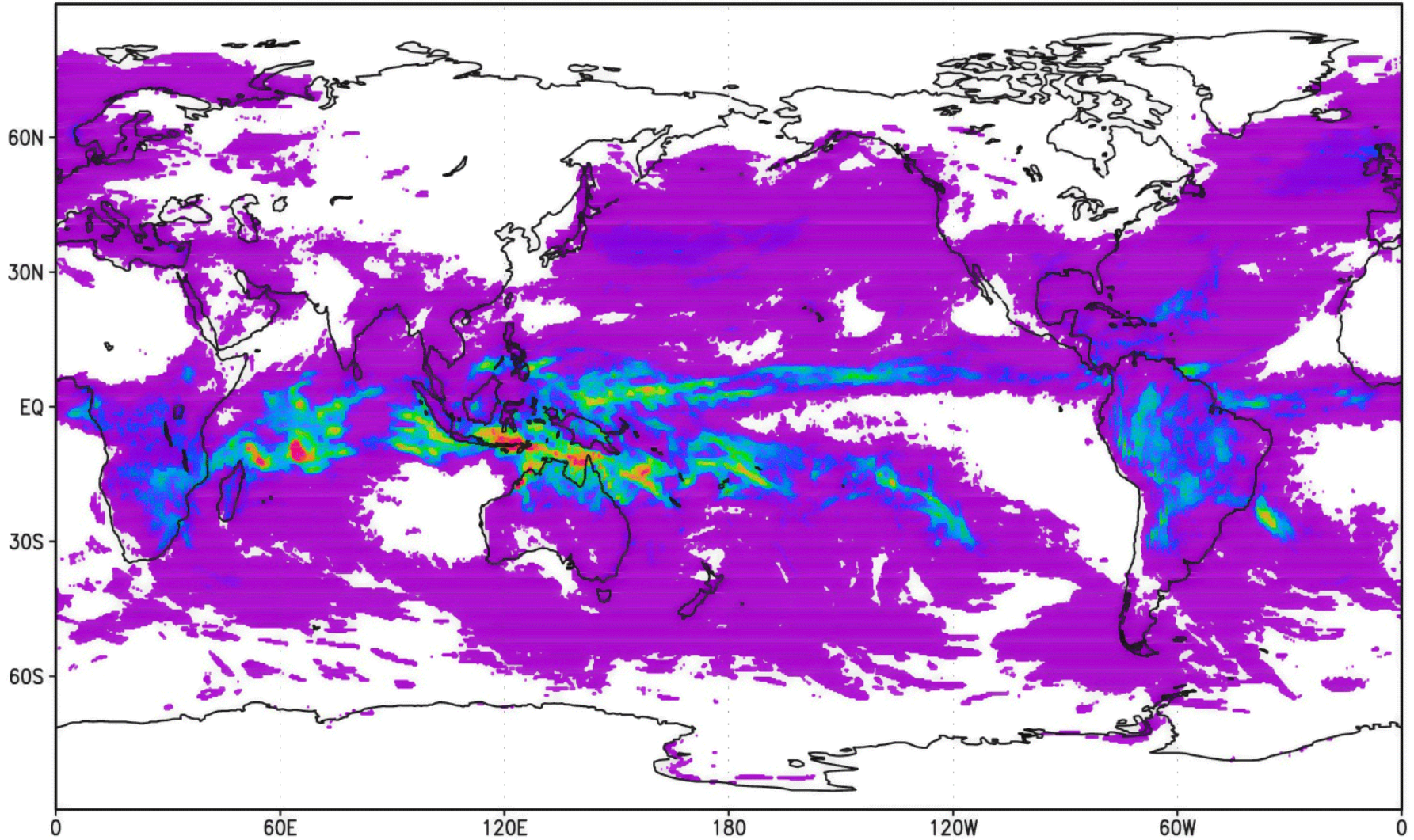
Planned (part of the COMBINE EC project):

- Past Control Run and Historical (1850-2005) Run
- Idealized 1%/yr simulation
- RCP4.5 and RCP8.5 simulations

# Mean JAN Precipitation Global 30km Resolution

Mean Jan convective precipitation (mm/day) T318

INGV - Istituto Nazionale di Geofisica e Vulcanologia - Italy



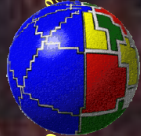


# CIRCE

*Climate Change and Impact ResearCh:  
the Mediterranean Environment*

**An FP6 Project of the European Union**

Profisica e Vulcanologia - Italy

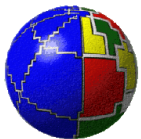


INGV - Istituto Nazio

**Chair: Antonio Navarra and Laurence Tubiana**  
[www.circeproject.eu](http://www.circeproject.eu)

# Evolution of Computational Resources

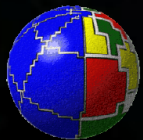
| Grid Spacing                              | Effective Resolution (km) | Cost relative to 2005 models |
|---|---------------------------|------------------------------|
| 630                                       | 1350                      | 0.015                        |
| ~1975 Climate Models                      |                           |                              |
| 320                                       | 670                       | 0.12                         |
| 160                                       | 330                       | 1                            |
| ~2005 Climate Models                      |                           |                              |
| 110                                       | 220                       | 3.3                          |
| 50  | 110                       | 27                           |
| 26  | 60                        | 220                          |
| 17  | 40                        | 830                          |
| ~2005 Numerical Weather Prediction Models |                           |                              |
| 10  | 20                        | 3800                         |
| 4   | 8.5                       | 60,000                       |
| 1   | 2.1                       | 3,800,600                    |
| 0.5                                       | 1                         | 37,000,000                   |



# A new paradigm for numerical simulations

*Numerical experiments will be complex multi-institutional, transnational enterprises*

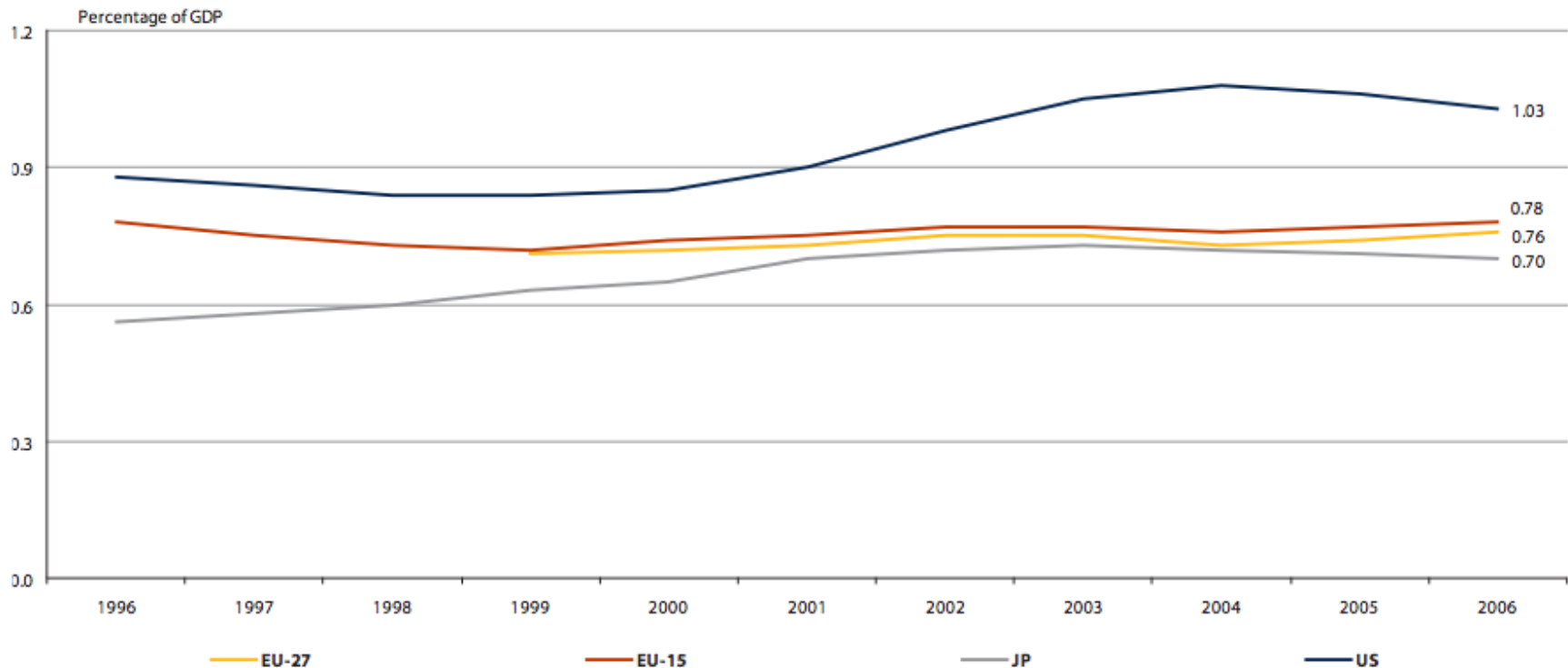
- **Concept Stage** – Definition of idea and objective, analysis of existing skills and resources
- **Scientific Case** – Definition of scientific objectives and goals, arguments for priority in terms of scientific values, relevance and impact
- **Technical Case** – Definition of methods and experimental planning, organization and governance of the consortium, exploitation strategy
- **Detailed Multiyear Planning** – Detailed definition of targets and responsibilities in the consortium, phasing of experimental and analysis systems and archiving, decommissioning strategy



*Welcome to the era of Industrial Computing*

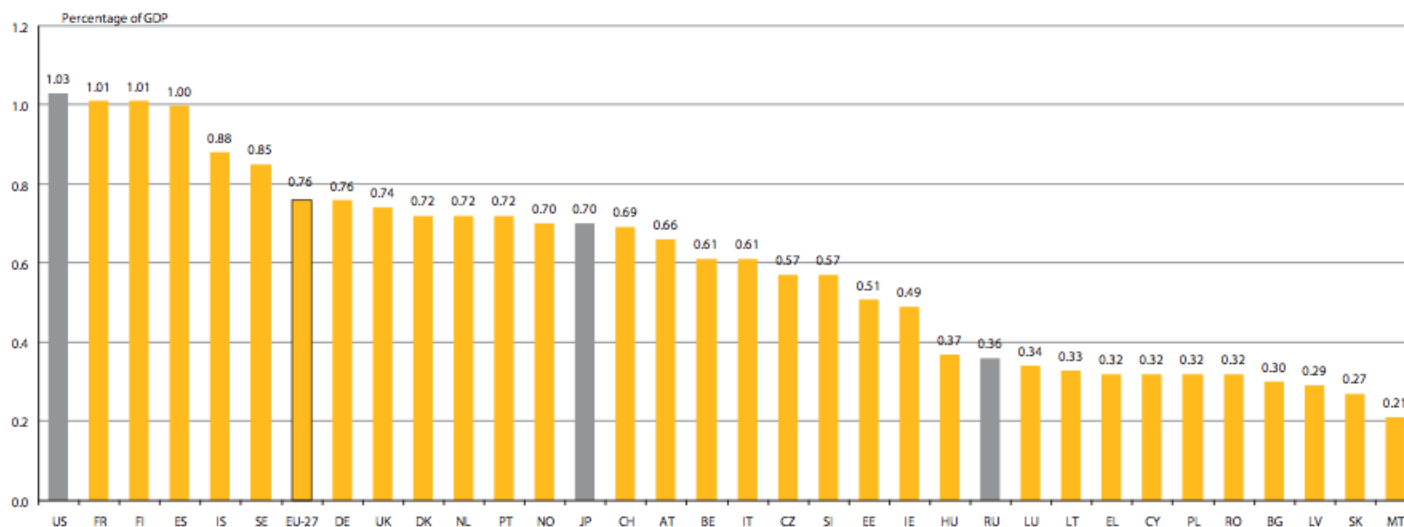
# R&D Trends

**Figure 1.1:** Total GBAORD as a percentage of GDP, EU-15, EU-27, Japan and the United States, 1996–2006

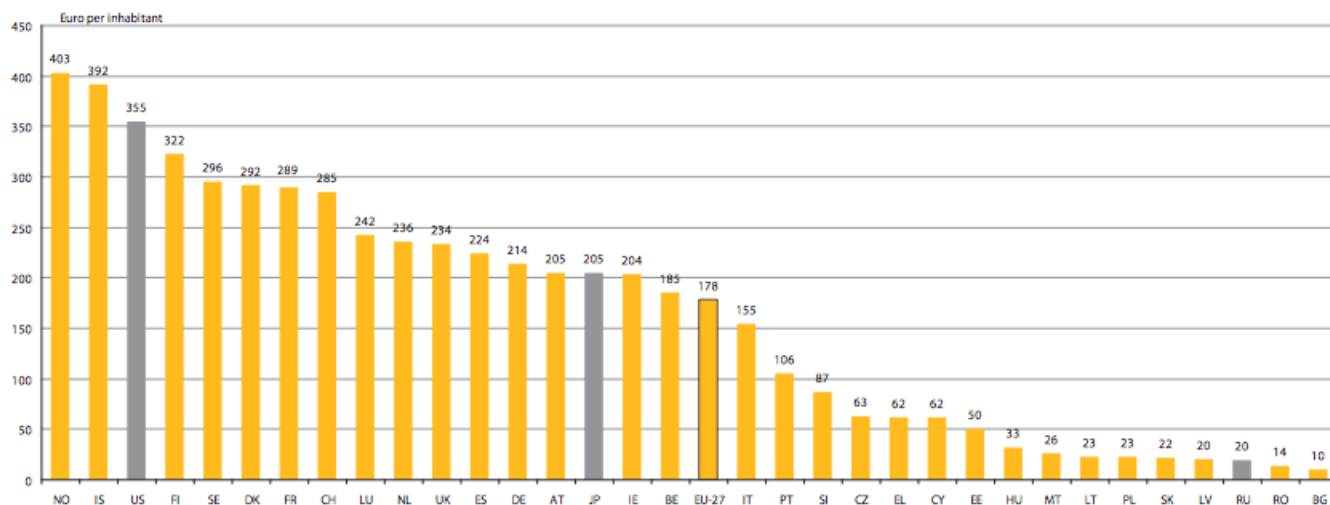


*GBAORD:*  
*government budget appropriations or outlays on research and development*

**Figure 1.2: Total GBAORD as a percentage of GDP, EU-27 and selected countries, 2006**

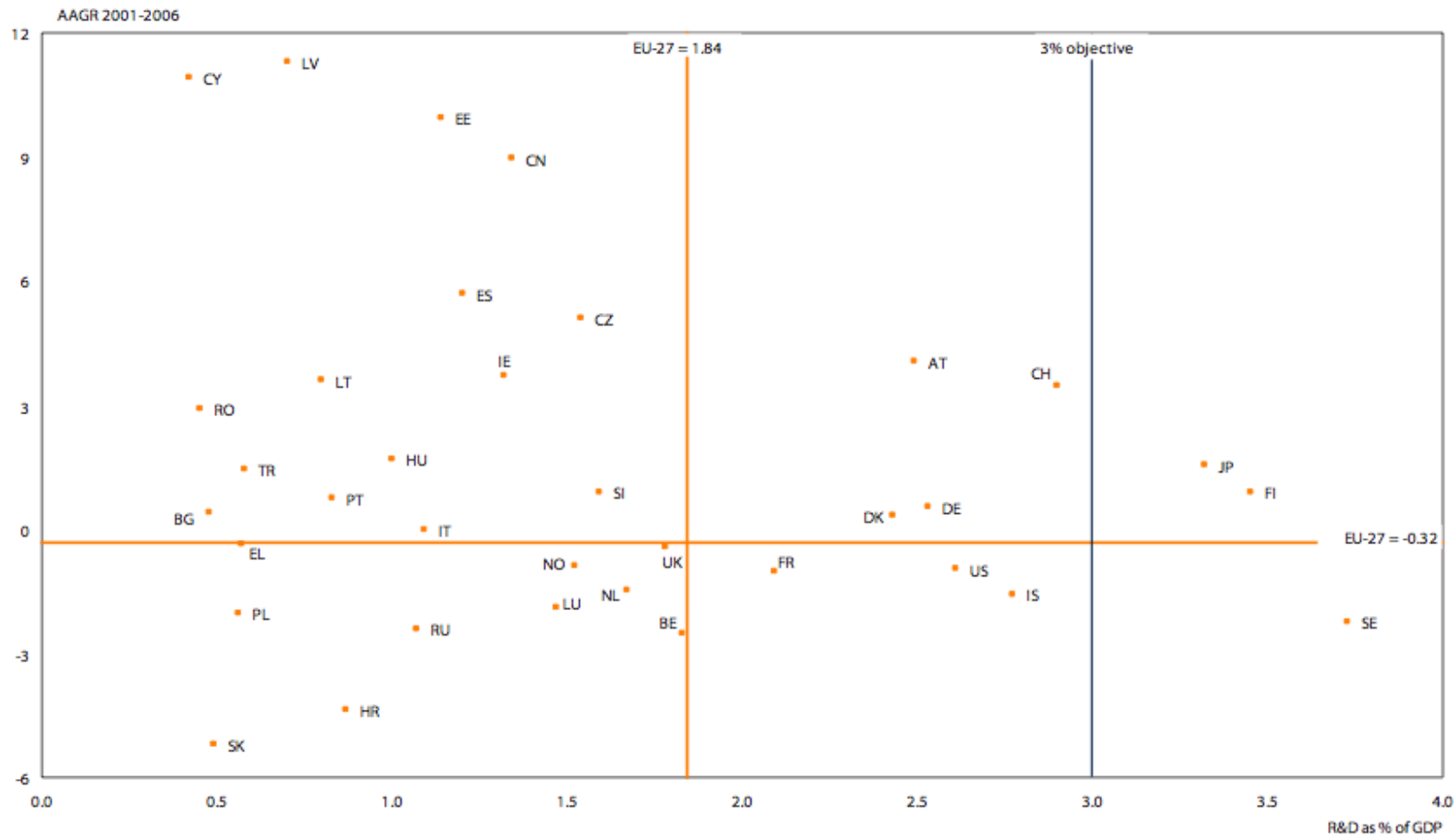


**Figure 1.4: Total GBAORD in EUR per inhabitant, EU-27 and selected countries, 2006**



# Evolution of R&D Expenditure

**Figure 2.2:** R&D expenditure as a percentage of GDP in 2006 and average annual growth rate (AAGR) 2001–2006<sup>(1)</sup>, all sectors, EU-27 and selected countries



**Table 1.6:** Total GBAORD in EUR million and by socio-economic objectives as a percentage of total GBAORD, EU-27 and selected countries, 2006

|              | Exploration and exploitation of the earth | Infrastructure and general planning of land-use | Control and care of the environment | Protection and improvement of human health | Production, distribution and rational utilization of energy | Agricultural production and technology | Industrial production and technology | Social structures and relationships | Exploration and exploitation of space | Research financed from GUF | Non-oriented research | Other civil research | Defence | Total civil GBAORD | Total GBAORD in mio eur |
|--------------|---|---|-------------------------------------|--|---|--|--------------------------------------|-------------------------------------|---------------------------------------|----------------------------|-----------------------|----------------------|---------|--------------------|-------------------------|
| <b>EU-27</b> | 1.6 s                                     | 1.8 s   | 2.5 s                               | 7.4 s                                      | 2.6 s   | 3.3 s                                  | 10.4 s                               | 3.5 s                               | 4.6 s                                 | 30.3 s                     | 17.1 s                | 1.8 s                | 13.2 s  | 86.8 s             | 87 840 s                |
| BE           | 0.6                                       | 0.8   | 2.2                                 | 1.9  | 1.9   | 1.3                                    | 33.3                                 | 4.1                                 | 10.1                                  | 17.1                       | 23.9                  | 2.6                  | 0.3     | 99.7               | 1 946                   |
| BG           | :   | :   | :                                   | :  | :   | :                                      | :                                    | :                                   | :                                     | :                          | :                     | :                    | :       | :                  | 75                      |
| CZ           | 2.1                                       | 3.8   | 2.6                                 | 6.8  | 2.4   | 4.9                                    | 11.8                                 | 2.5                                 | 0.7                                   | 26.4                       | 26.8                  | 6.0                  | 3.1     | 96.9               | 646                     |
| DK           | 0.7                                       | 0.7   | 1.7                                 | 8.5  | 2.1   | 5.9                                    | 6.4                                  | 6.5                                 | 1.9                                   | 44.3                       | 19.2                  | 1.5                  | 0.7     | 99.3               | 1 587                   |
| DE           | 1.8 i                                     | 1.8 i   | 3.1 i                               | 4.5 i                                      | 2.9 i   | 2.3 i                                  | 12.6 i                               | 3.5 i                               | 4.9 i                                 | 39.2 i                     | 16.9 i                | 0.6 i                | 6.5 i   | 93.5 i             | 17 608                  |
| EE           | 1.5 e                                     | 7.0 e   | 5.8 e                               | 9.3 e                                      | 3.1 e   | 10.3 e                                 | 5.2 e                                | 7.6 e                               | 0.0 e                                 | 0.0 e                      | 44.7 e                | 4.4 e                | 1.0 e   | 99.0 e             | 67 e                    |
| IE           | 2.6                                       | 0.5   | 0.8                                 | 5.5  | 0.0   | 9.8                                    | 9.3                                  | 11.1                                | 0.0                                   | 57.4                       | 2.9                   | 0.0                  | 0.0     | 100                | 858                     |
| EL           | 3.4                                       | 2.0   | 3.1                                 | 7.1  | 2.1   | 6.0                                    | 10.3                                 | 4.7                                 | 2.0                                   | 47.9                       | 9.3                   | 1.7                  | 0.5     | 99.5               | 685                     |
| ES           | 1.2                                       | 4.3   | 3.7                                 | 10.5                                       | 2.7   | 6.2                                    | 19.5                                 | 3.1                                 | 2.9                                   | 18.4                       | 7.3                   | 4.0                  | 16.2    | 83.8               | 9 799                   |
| FR           | 0.7 p                                     | 0.7 p   | 2.2 p                               | 4.8 p                                      | 3.6 p   | 1.2 p                                  | 5.9 p                                | 0.5 p                               | 7.1 p                                 | 21.7 p                     | 26.6 p                | 2.6 p                | 22.4 p  | 77.6 p             | 18 225 p                |
| IT           | 2.3                                       | 1.0   | 2.6                                 | 10.3                                       | 4.0   | 4.0                                    | 11.7                                 | 5.2                                 | 9.5                                   | 41.8                       | 6.2                   | 0.0                  | 1.4     | 98.6               | 9 099                   |
| CY           | 1.6                                       | 1.3   | 1.1                                 | 6.1  | 0.4   | 21.0                                   | 2.7                                  | 7.9                                 | 0.0                                   | 27.0                       | 31.0                  | 0.0                  | 0.0     | 100                | 47                      |
| LV           | 0.6                                       | 1.6   | 2.8                                 | 6.9  | 3.4   | 18.7                                   | 16.2                                 | 8.1                                 | 0.3                                   | :                          | 41.1                  | :                    | 0.3     | 99.7               | 46                      |
| LT           | 2.6                                       | 4.2   | 9.3                                 | 9.9  | 3.2   | 8.4                                    | 12.2                                 | 32.3                                | :                                     | :                          | :                     | 17.0                 | 0.9     | 99.1               | 78                      |
| LU           | 0.4                                       | 3.2   | 4.0                                 | 8.4  | 0.6   | 2.6                                    | 22.1                                 | 15.8                                | 0.4                                   | 18.8                       | 20.4                  | 3.1                  | 0.0     | 100.0              | 114                     |
| HU           | 2.9                                       | 2.1   | 9.7                                 | 13.1                                       | 10.4  | 16.4                                   | 19.6                                 | 9.1                                 | 2.3                                   | 9.1                        | 5.0                   | 0.3                  | 0.1     | 99.9               | 329                     |
| MT           | 0.0                                       | 0.8   | 0.0                                 | 0.0  | 0.0   | 6.3                                    | 0.0                                  | 4.2                                 | 0.0                                   | 86.1                       | 1.3                   | 1.3                  | 0.0     | 100                | 10.5                    |
| NL           | 0.3                                       | 3.8   | 1.9                                 | 4.5  | 2.1   | 5.3                                    | 10.9                                 | 1.8                                 | 3.1                                   | 47.1                       | 10.0                  | 7.1                  | 2.1     | 97.9               | 3 858                   |
| AT           | 2.0 i                                     | 1.4 i   | 1.6 i                               | 3.8 i                                      | 0.7 i   | 1.9 i                                  | 12.6 i                               | 1.9 i                               | 0.2 i                                 | 60.7 i                     | 13.2 i                | 0.0 i                | 0.0 i   | 100 i              | 1 692 i                 |
| PL           | 0.9                                       | 0.7   | 1.3                                 | 1.5  | 0.7   | 0.7                                    | 10.8                                 | 0.5                                 | 0.1                                   | 4.8                        | 76.9                  | 0.2                  | 0.9     | 99.1               | 858                     |
| PT           | 1.2 p                                     | 6.6 p   | 3.8 p                               | 7.0 p                                      | 0.9 p   | 8.1 p                                  | 16.9 p                               | 3.7 p                               | 0.3 p                                 | 38.5 p                     | 9.2 p                 | 3.2 p                | 0.6 p   | 99.4 p             | 1 116 p                 |
| RO           | 2.3                                       | 3.0   | 5.1                                 | 5.7  | 2.3   | 9.4                                    | 22.1                                 | 11.9                                | 1.4                                   | :                          | 13.8                  | 19.8                 | 3.2     | 96.8               | 309                     |
| SI           | 0.0                                       | 1.6   | 1.6                                 | 3.7  | 0.9   | 2.3                                    | 22.8                                 | 2.3                                 | 0.0                                   | 4.5                        | 49.6                  | 9.2                  | 1.6     | 98.4               | 173                     |
| SK           | 1.0                                       | 7.3   | 0.0                                 | 5.0  | 0.1   | 8.1                                    | 8.9                                  | 2.5                                 | :                                     | 26.0                       | 32.6 i                | 1.7                  | 6.6 i   | 93.4 i             | 120                     |
| FI           | 1.2                                       | 2.0   | 1.6                                 | 6.2  | 4.4   | 5.8                                    | 27.2                                 | 5.5                                 | 1.7                                   | 25.6                       | 16.2                  | :                    | 2.8     | 97.2               | 1 694                   |
| SE           | 0.7 p                                     | 4.0 p   | 1.8 p                               | 1.2 p                                      | 3.6 p   | 2.2 p                                  | 5.7 p                                | 4.5 p                               | 0.9 p                                 | 45.1 p                     | 13.6 p                | :                    | 16.8    | 83.2               | 2 675                   |
| UK           | 2.7 p                                     | 0.8 p   | 1.8 p                               | 14.1 p                                     | 0.2 p   | 3.1 p                                  | 1.1 p                                | 5.3 p                               | 2.2 p                                 | 21.6 p                     | 18.6 p                | 0.4 p                | 28.3 p  | 71.7 p             | 14 124 p                |
| IS           | :   | 4.7   | 0.4                                 | 10.9                                       | 1.5   | 21.1                                   | 0.9                                  | 7.6                                 | :                                     | 40.4                       | 12.5                  | 0.0                  | 0.0     | 100                | 117                     |
| NO           | 2.5                                       | 2.4   | 1.9                                 | 11.3                                       | 3.3   | 8.5                                    | 7.9                                  | 6.3                                 | 2.1                                   | 34.9                       | 12.9                  | :                    | 5.9     | 94.1               | 1 869                   |
| CH           | 0.1 i                                     | 0.3 i   | 0.1 i                               | 1.3 i                                      | 1.0 i   | 2.2 i                                  | 1.0 i                                | 2.2 i                               | 4.5 i                                 | 59.6 p                     | 9.1 i                 | 17.7 i               | 0.6 i   | 99.4 i             | 2 123                   |
| JP           | 1.8 i                                     | 4.1 i   | 0.8 i                               | 3.9 i                                      | 15.2 i  | 3.4 i                                  | 7.3 i                                | 0.7 i                               | 6.8 i                                 | 34.2 i                     | 16.7 i                | :                    | 5.1 i   | 94.9 i             | 24 478 i                |
| RU           | :   | :   | :                                   | :  | :   | :                                      | :                                    | :                                   | :                                     | :                          | :                     | :                    | :       | :                  | 2 854                   |
| US           | 0.8 i                                     | 1.3 i   | 0.5 i                               | 21.8 i                                     | 0.9 i   | 2.0 i                                  | 0.3 i                                | 1.3 i                               | 7.6 i                                 | :                          | 5.5 i                 | 0.0                  | 57.9 i  | 42.1 i             | 108 330 i               |

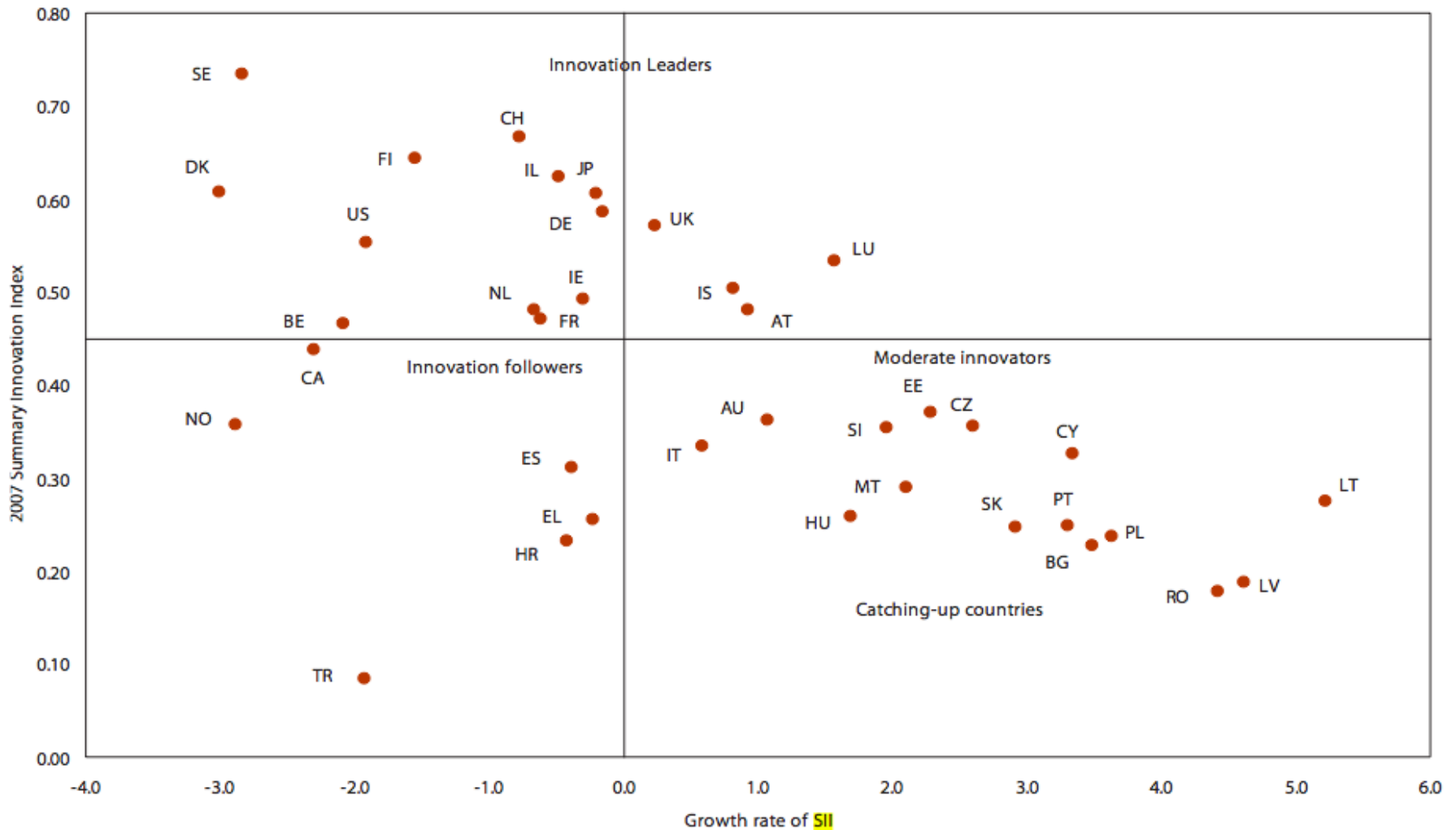
**Table 2.3: R&D expenditure in EUR million and average annual growth rate (AAGR), by sector of performance, EU-27 and selected countries, 2001–2006**

|              | All sectors |            |                   | Business enterprise sector |            |                   | Government sector |           |                   | Higher education sector |           |                   |
|--------------|-------------|------------|-------------------|----------------------------|------------|-------------------|-------------------|-----------|-------------------|-------------------------|-----------|-------------------|
|              | 2001        | 2006       | AAGR<br>2001-2006 | 2001                       | 2006       | AAGR<br>2001-2006 | 2001              | 2006      | AAGR<br>2001-2006 | 2001                    | 2006      | AAGR<br>2001-2006 |
| <b>EU-27</b> | 178 549 s   | 213 127 s  | 3.6 s             | 115 689 s                  | 135 716 s  | 3.2 s             | 23 570 s          | 28 777 s  | 4.1 s             | 37 914 s                | 46 666 s  | 4.2 s             |
| BE           | 5 373       | 5 798 p    | 1.5 p             | 3 921                      | 3 934 p    | 0.1 p             | 331               | 500 p     | 8.6 p             | 1 059                   | 1 291 p   | 4.0 p             |
| BG           | 71          | 121        | 11.3              | 15                         | 31         | 16.2              | 48                | 78        | 10.2              | 9                       | 12        | 5.9               |
| CZ           | 832         | 1 761      | 16.2              | 501                        | 1 165      | 18.4              | 197               | 309       | 9.4               | 130                     | 279       | 16.5              |
| DK           | 4 278       | 5 349 p    | 4.6 p             | 2 934                      | 3 560 p    | 3.9 p             | 503               | 360 p     | -6.5 p            | 809                     | 1 396 p   | 11.5 p            |
| DE           | 52 002      | 58 848 p   | 2.5 p             | 36 332                     | 41 148     | 2.5               | 7 146 i           | 8 100 p   | 2.5 p             | 8 524                   | 9 600 p   | 2.4 p             |
| EE           | 49          | 151 p      | 25.3 p            | 16                         | 67 p       | 32.5 p            | 7                 | 20        | 23.6              | 25                      | 61        | 20.0              |
| IE           | 1 284       | 2 311 p    | 12.5 p            | 900                        | 1 560 p    | 11.6 p            | 104               | 150       | 7.6               | 280                     | 601       | 16.5              |
| EL           | 852         | 1 223 e    | 7.5 e             | 278                        | 367 e      | 5.7 e             | 188               | 254 e     | 6.3 e             | 383                     | 585 e     | 8.9 e             |
| ES           | 6 227       | 11 815     | 13.7              | 3 261                      | 6 558      | 15.0              | 989               | 1 971     | 14.8              | 1 925 e                 | 3 266     | 11.1              |
| FR           | 32 887      | 37 844 p   | 2.8 p             | 20 782 b                   | 23 942 p   | 2.9 p             | 5 432             | 6 546 p   | 3.8 p             | 6 217                   | 6 875 p   | 2.0 p             |
| IT           | 13 572      | 15 599     | 3.5               | 6 661                      | 7 856      | 4.2               | 2 493             | 2 701     | 2.0               | 4 418                   | 4 712 b   | 1.6 b             |
| CY           | 27          | 62 p       | 17.6 p            | 5                          | 14 p       | 21.0 p            | 12                | 18 p      | 7.0 p             | 7                       | 26 p      | 29.1 p            |
| LV           | 38          | 112        | 24.4              | 14                         | 57         | 32.7              | 8                 | 17        | 15.9              | 16                      | 39        | 19.5              |
| LT           | 91          | 191        | 15.9              | 27                         | 53         | 14.9              | 36                | 44        | 3.8               | 29                      | 94        | 26.8              |
| LU           | 364         | 497 pe     | 5.3 pe            | 337                        | 422 e      | 3.8 e             | 26                | 63 p      | 15.8 p            | 1                       | 12 p      | 54.0 p            |
| HU           | 548 i       | 900        | 10.4              | 220 i                      | 435 i      | 14.6 i            | 142 i             | 228 i     | 10.0 i            | 141 i                   | 219 i     | 9.2 i             |
| MT           | 12          | 28 p       | 23.5 p            | 3                          | 17 p       | 55.2 p            | 2                 | 1         | -9.3              | 7                       | 9         | 7.2               |
| NL           | 8 075       | 8 910 pe   | 2.0 pe            | 4 712                      | 5 134 p    | 1.7 p             | 1 114             | 1 260 i   | 2.5 i             | 2 184                   | :         | :                 |
| AT           | 4 684       | 6 423 e    | 8.2 e             | 3 131                      | 4 284 e    | 8.2 e             | 266               | 325 e     | 5.1 e             | 1 266                   | 1 689 e   | 7.5 e             |
| PL           | 1 323       | 1 513      | 2.7               | 474                        | 477        | 0.1               | 414               | 560       | 6.2               | 433                     | 469       | 1.6               |
| PT           | 1 038       | 1 201      | 3.7               | 330                        | 462        | 8.8               | 216               | 176       | -5.0              | 381                     | 425       | 2.8               |
| RO           | 177         | 444        | 20.2              | 109                        | 215        | 14.6              | 48                | 144       | 24.6              | 20                      | 79        | 31.5              |
| SI           | 341         | 484        | 7.2               | 197                        | 291        | 8.1               | 83                | 119       | 7.4               | 55                      | 73        | 5.7               |
| SK           | 149         | 217        | 7.7               | 101                        | 93         | -1.5              | 35 i              | 71 i      | 14.9 i            | 13                      | 52        | 31.2              |
| FI           | 4 619       | 5 761      | 4.5               | 3 284                      | 4 108      | 4.6               | 471               | 539       | 2.7               | 834                     | 1 079     | 5.3               |
| SE           | 10 511 i    | 11 691     | 2.2               | 8 118 i                    | 8 754      | 1.5               | 297 i             | 525       | 12.1              | 2 085                   | 2 387     | 2.7               |
| UK           | 29 403      | 34 037     | 3.0               | 19 260 b                   | 20 985     | 1.7               | 2 949 b           | 3 401     | 2.9               | 6 671                   | 8 892     | 5.9               |
| IS           | 261         | 364        | 8.7               | 153                        | 187        | 5.1               | 52                | 86        | 13.1              | 49                      | 80        | 13.0              |
| NO           | 3 037       | 4 071      | 6.0               | 1 814                      | 2 204      | 4.0               | 444               | 637       | 7.5               | 780                     | 1 229     | 9.5               |
| CH           | 6 852       | 8 486      | 5.5               | 5 065                      | 6 257      | 5.4               | 90 bi             | 91 i      | 0.2 i             | 1 566                   | 1 943     | 5.5               |
| HR           | 271         | 297        | 2.4               | 115                        | 109        | -1.4              | 60                | 79        | 7.0               | 95                      | 109       | 3.5               |
| TR           | 1 172       | 2 432      | 15.7              | 395                        | 901        | 17.9              | 86                | 284       | 26.9              | 690                     | 1 248     | 12.6              |
| CN           | 14 063      | 30 002     | 16.4              | 8 499                      | 21 325     | 20.2              | 4 183             | 5 912     | 7.2               | 1 381                   | 2 765     | 14.9              |
| JP           | 143 015     | 121 831    | -3.9              | 105 364                    | 93 137     | -3.0              | 13 637            | 10 100    | -7.2              | 20 687                  | 16 330    | -5.7              |
| RU           | 4 025       | 8 466      | 16.0              | 2 829                      | 5 643      | 14.8              | 978               | 2 285     | 18.5              | 210                     | 517       | 19.8              |
| US           | 310 205 i   | 273 772 pi | -2.5 pi           | 225 566 i                  | 192 584 pi | -3.1 pi           | 35 013 i          | 30 462 pi | -2.7 pi           | 37 642 i                | 39 098 pi | 0.8 pi            |



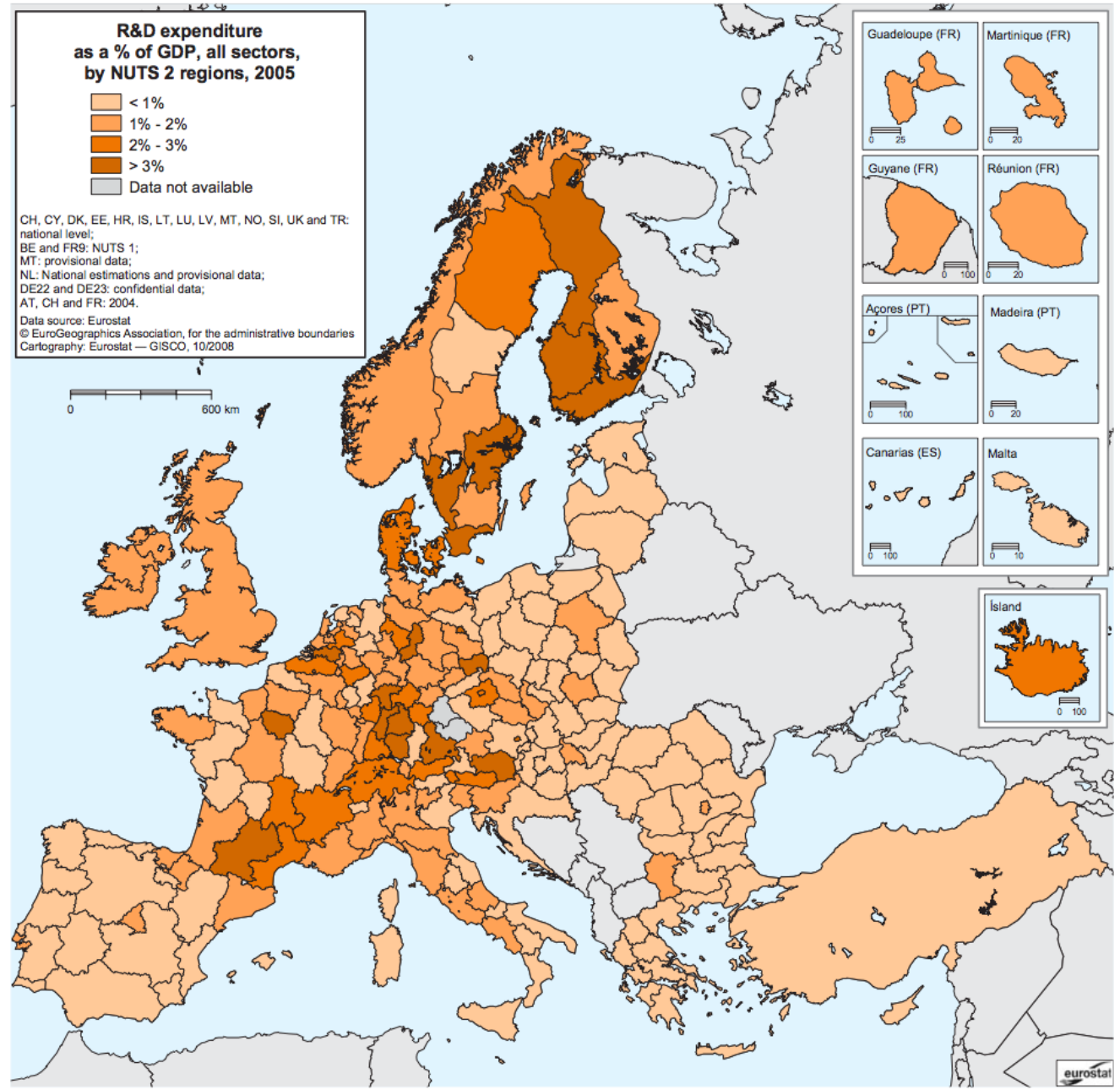
# Summary Innovation Index

Figure 5.1: Summary Innovation Index (SII) in 2007 and growth rate of SII, EU-27 and selected countries

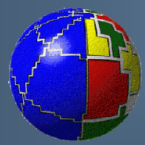


Map 2.12: R&D expenditure as a percentage of GDP, all sectors, 2005 - NUTS 2

# Regional R&D



INGV - Istituto Nazionale di Geofisica e Vulcanologia - Italy



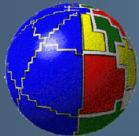
# Sustaining and directing the research effort

Funding for Earth Systems research is stationary or decreasing.

Single investigator programs (NSF or ERC) are too small to engage global issues.

Research spending from defense budgets and private sector entities – is still not keyed to climate and low carbon research.

Investments in climate research and low carbon technologies are not growing



# A new international research paradigm

***We need to identify the new questions.*** What are the big scientific and technological questions that will make a real difference to policy and investment decisions in the coming decade, and that can drive the research agenda of the next generation of researchers and scientists?

***We need to mobilize new sources of funding.*** We need to be able to articulate the scale of funding needed. What is the scale of that funding? How does it compare to other efforts to accomplish other advancements in knowledge and technology?

***We need new global institutional solutions*** to deliver the support this research deserves. What forms of global public-private partnerships do we need to ensure the private sector invests for the long term? What institutional arrangement should we set in place?

